

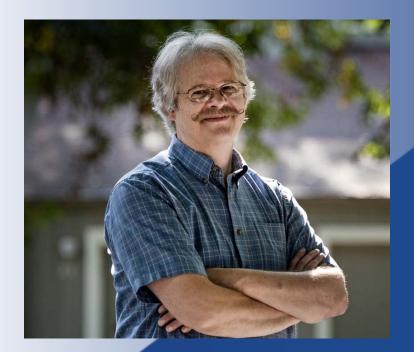
Industrial Fan Systems Virtual INPLT Training & Assessment

Session 7



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Fan Virtual INPLT Facilitator



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- William (Bill) Hunter, PE, Airclean Systems, Seattle WA
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- William (Bill) W.T. Corey, Corey Consultancy, Surrey England
- US Department of Energy , Advanced Manufacturing Office
- Oak Ridge National Laboratory
- United Nations Industrial Development Organization
- Many industrial clients both in the US and internationally



Safety and Housekeeping

Safety Moment

- $\circ~$ Fans can be dangerous, and caution should be used around fan systems
- Accidents can be life-threatening
- You are welcome to ask questions at any time during the webinar
- When you are not asking a question, please <u>MUTE</u> your mic and this will provide the best sound quality for all participants
- We will be recording all these webinars and by staying on-line and attending the meeting you are giving your consent to be recorded
 - $\circ~$ A link to the recorded webinars will be provided, afterwards





Fan system Virtual INPLT Agenda

- Week 1 Industrial Fan Systems Fundamentals and Introduction to MEASUR
- Week 2 Fan and system curves, Fan types
- Week 3 Fan affinity laws, Fan system controls
- Week 4 Creating a fan performance measurement plan & selecting measurement planes
- Week 5 Pressure considerations, Sizing ducts and estimating losses, Optimization techniques
- Week 6 Psychrometrics and air density for fan systems, System effect in fan systems
- Week 7 Fan system optimization strategies, Fan system evaluation with MEASUR
- Week 8 Industrial Fan System VINPLT Wrap-up Presentations





Class participants will:

- 1. List 4 common fan system optimization (FSO) techniques
- 2. Discuss advantages and disadvantages of common FSO techniques
- 3. Develop a list of relevant FSO strategies;
- 4. Describe heat recovery opportunities and strategies;
- 5. Analyze field data to establish MEASUR inputs;
- 6. Use MEASUR to analyze the optimization potential of fan systems;





Other fan application training opportunities

For more in-depth training, go to AMCA.org for self-paced, fully interactive courses:

- AC motors in fan systems
- Fan power law
- Psychrometrics for fan systems
- Fan affinity laws simplified
- Advanced fan affinity laws
- Fan system controls
- In-situ fan measurements (ISO 5802)
- Calculating flow rate
- Heat recovery in fan systems
- Fan energy index (FEI)

The AMCA website also has loads of pre-recorded webinars you can choose from





Fan optimization techniquess



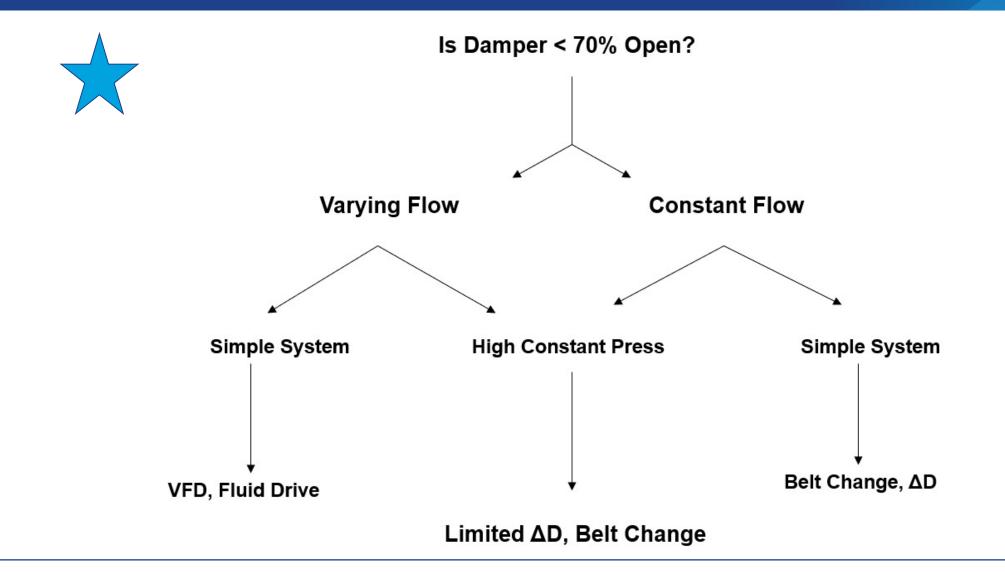
Fan System Optimization

- Overview
- Change Fan Speed (various methods)
 - Affinity Laws
- Modify Impeller (tip/detip)
- Replace Impeller or Fan
- Improve fan control





Optimization Method Flow Chart







Upgrade / Replace Impeller

+ Improve efficiency

- + Closely match flow and pressure to process requirements
- + Much lower cost than replacing the whole fan
- Specialty item that not all fan vendors can easily supply
- Best done in conjunction with a field performance test

Best suited for over 200 hp and where new impeller design would be more efficient, or have other advantages such as reduced impeller wear





Usually used on fans larger than 200 hp

- + Can trim or boost flow to match process requirements
- + Inexpensive compared to replacing the impeller or the fan
- Should be done in coordination with fan supplier
- Before tipping the fan, need to check for adequate space in the housing
- Impeller will need to be re-balanced





Replace Fan

- + Can be sized to meet the load
- \$\$ New base
- \$\$ Modification
- \$\$ Ductwork may require modification
- Downtime

Best suited for aging or deteriorating fans.





New belt drive ratio

- + Inexpensive
- + Reversible
- + Ratio can be changed later if needed
- Preparation required
- Performance tests needed

Best suited when there is an existing belt drive, the load is constant* and the fan is oversized with a damper used as a control mechanism

* If the load is variable, then you may be able to change the belt ratio and utilize a much smaller VFD





Convert to belt drive

Best suited:

•when the current fan is oversized and has a direct drive motor operating at 100 hp or less.

If the load is constant and or if a VFD is too expensive or otherwise unsuitable for the system

- + Fan speed can be changed
- + Less costly than a VFD, but still an expensive proposition
- + Best for steady loads
- Fan bearings may not withstand the lateral force or belt thrust
- A new base may be required for the motor or fan
- Belts require additional maintenance





Best suited for systems with variable flow rates

- + Fan output can be exactly matched to process needs
- + No mechanical changes needed
- + Often very cost effective
- + Can easily replace throttle control
- + Can be used to over speed the fan motor
- Costly & slightly less reliable for medium voltage motors
- Can cause problems with electrical systems
- Additional space is needed in the electrical room
- Air conditioning is needed in the electrical room





Variable Frequency Drive (VFD) (cont.)

- Very sensitive to electrical power quality
- Best to use a specialized cable
- Purchase requires time and expertise
- The VFD vendor needs to know:
 - starting torque of the fan,
 - age and condition of the fan motor, and
 - distance between the fan and electrical room

DO NOT USE A VFD with a system already at full capacity, under a steady load, or when there are only minor flow variations





Optimization Techniques for Existing Systems (cont.)

6. Fluid Couplings

- + Can be used for larger fan motors greater than 500 kW where a belt drive can't be used
- \$\$ Can be expensive and inefficient
- Most fluid couplings in service were installed years ago, advances in VFD technology have made fluid couplings almost obsolete

Best suited to vary the speed on larger motors

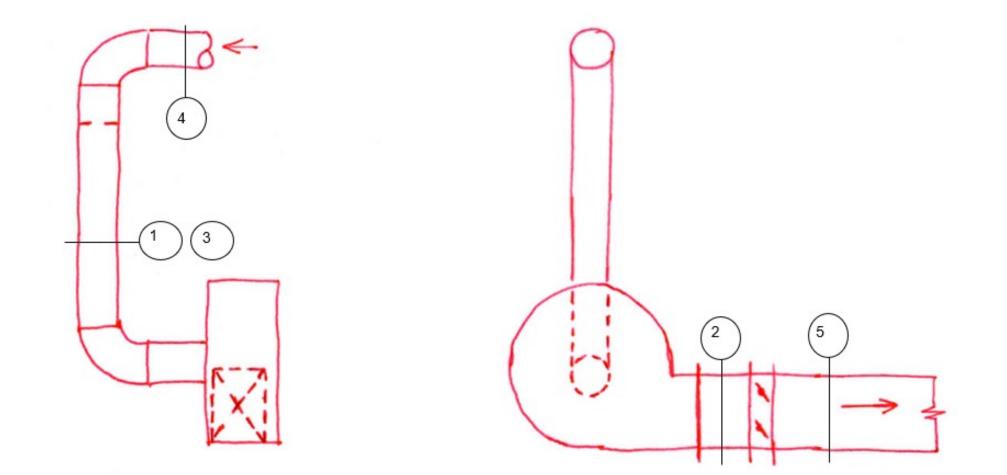




Fan system evaluation with MEASUR



Measurement plan for combustion air blower







Fan System Field Data Collection Sheet initial <u>RW</u> test # <u>1</u> 1 of 3 File 1215									
	COMBUSTIO	N AIR E	LOWER						
Customer									
Tester RW /FP	Test Start Tin ໆ:00	ne 2/19/96	Test End Time	10:10					
PROCESS CONDITIONS 5 teachy 59% Dryer load - Typical									
Hours operation									
MOTOR NAME PLATE D	ATA								
Manufacturer SIEMEN	2	Model/Fra	me /445 EFF /445	57					
HP rpm	85 Volts 46	FLA	15 PF 89	EFF 95.4					





FAN NAME PLATE DATA	
Manufacturer	Model
CHAMPION FAN	385 HPR
Impeller Flat radial	serial 266 V 92-1
rpm 2473	Impeller diameter
Notes (age and general condition)	1
Approx 15 years old	. good condition
SYSTEM EFFECT FACTORS Estimate as per Fans	and Systems, AMCA Publication 201.
SEF1 N/A	
	,

AMBIENT CONDITIONS		DB	WB	P _{Barometric}
Does $P_{Barometric}$ require altitude correction? λ D	pre test	6 <i>5</i> [°] €	50°F	29,45 ^{in. Hg}
Altitude	post test	67 °F	5°°	in. Hg 29.45





Fan System Field Data Collection Sheet	initial \underline{PW} test # _/ 2 of 3 file 1215					
FAN AND MOTOR		А	В	С		
Motor rpm /787	Volts	460	458	462		
Fan rpm 2473	Amps	104	104.4	104.2		
Drive type BELT	or kW					
TEST PLANES (show on sketch)	DB	WB	Area	P (local)		
Plane #1 Fan Inlet SAME BELOW ORIFICE #3	°F 127.5	°F 71.7	£.76/	in. H2O -6,850		
Plane #2 Fan Outlet	155°F	۴	ft ² or 1 x w 1, 611	in. H₂O 35,60		
Plane #3 Traverse SAME AS #1	127.5	71.7°F	ft ² or 1 x w 2.76/	in. H20 -6,850		
Plane #4 Upstream	127.5	71.7°F	ft ² or 1 x w Z , 761	in. H₂O -2.95		
Plane #5 Downstream	155°F	۴	ft ² or 1 x w 2,297	in. H ₂ O		
Plane #6	°F	°F	ft ² or I x w	in. H ₂ O		
	°F	°F	ft ² or I x w	in. H₂O		





TRAVERSE DATA velocity pressure in. w.g.										
	Points									
Ports	1	2	3	4	5	6	7	8	9	10
1	0,20	1.20	Z.50	0.90	0.20	-0.05	-0.04	6.35		
2	0.30	1.50	1.90	0.40	0.10	-0.01	0.03	0.65		
3	0.10	1.90	05.5	0.40	0.20	0.20	0.50	0.70		
4										
5							in.			
6										
7										
8										-
9										
10										





Directions: There are four steps in analyzing fan system field data:

- 1. Calculate or establish the density at the measurement planes.
- 2. Estimate the average air velocity and calculate flow rate at the traverse plane.
- 3. Translate the flow rate to other measurement planes and calculate velocity pressures at the other measurement planes.
- 4. Once the velocity pressures are known :





	Pv	Ps	Pt	ρ	v	Α	Q
Plane 1							
Plane 2							
Plane 3							
Plane 4							
Plane 5							
Plane 6							





- Estimate the average air velocity and calculate flow rate at the traverse plane:
- Calculate the root mean square of velocity pressure

$$P_{v3} = \left(\frac{\sum_{i=1}^{n} \sqrt{P_{v3i}}}{n}\right)^2$$





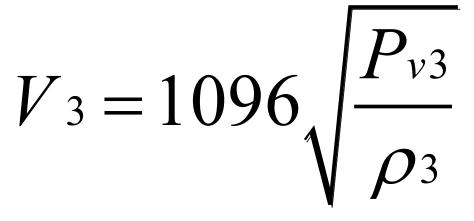
 A table like this can be used to sum up the square of the velocity pressure readings

Ports	1	2	3	4	5	6	7	8	9	10
1										
2	· ·									
3										
4										
5										
6										
7										
8										
9										
10										
Total	× 13			э D.						00
grand total										





 After finding the velocity pressure at plane 3, calculate the velocity at plane 3 and the flow rate.

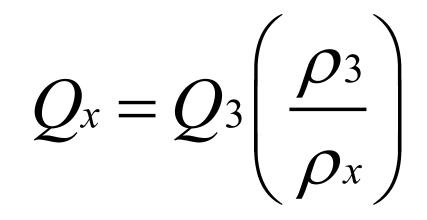


$$Q_3 = V_3 A_3$$





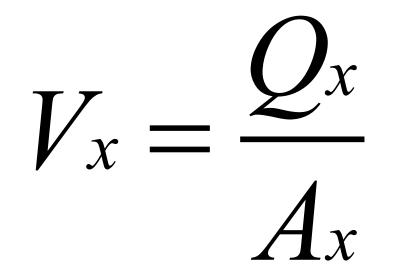
- Translate the flow rate to other measurement planes and calculate total pressure at other measurement planes:
 - Calculate the flow rate at the other planes.







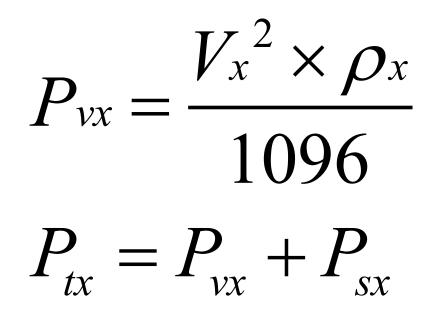
- Step 3 continued
 - Calculate the velocity at the other planes







- Step 3 continued
 - Calculate the velocity pressure and the total pressure at other planes







- Calculate the MEASUR inputs:
 - Calculate Ps the fan static pressure

$P_{s} = P_{s2} - P_{s1} - P_{v1}$

- Calculate the pressure required by the process
- Calculate the average amps and volts





Combustion Air Blower Performance: MEASUR Input

- 1. Complete the Data Collection Worksheet
- 2. Input flow traverse, pressure, and power findings into MEASUR
- 3. Use MEASUR to analyze the fan efficiency
- 4. Analyze optimization improvements





MEASUR Demo

Switch to live demo of MEASUR software





Heat recovery in fan systems



In many fan systems, the thermal energy being carried by the fluid far exceeds the electrical energy driving the fan motor. In all too many cases the energy is dumped to atmosphere or discarded.

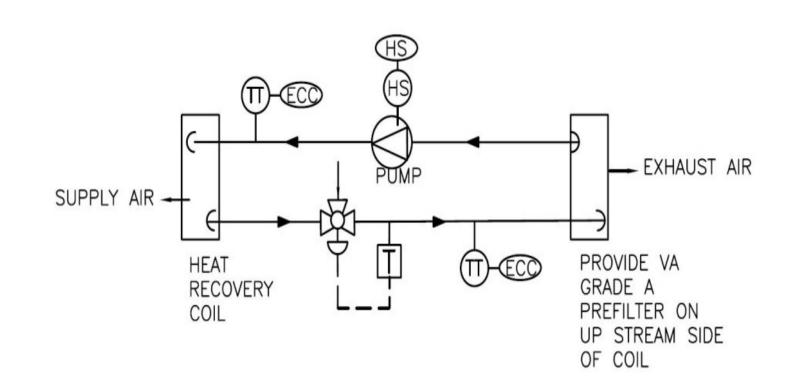
- Glycol Run-Around System
- Air-to-Air
 - Flat plate
 - Heat Pipes
 - Heat Wheel
- Air to Water
- Water to Air





Glycol Run-Around System

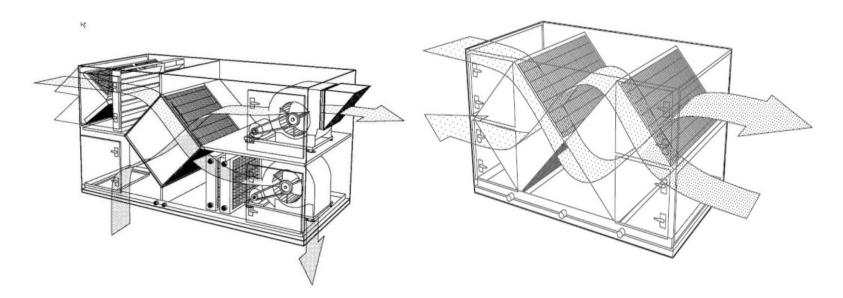
2







Air-to-Air – Flat plate



Make-up Air Unit

Double Pass Arrangement





Industrial Grade Air-to-Air 2 Pass HX with Steel Construction

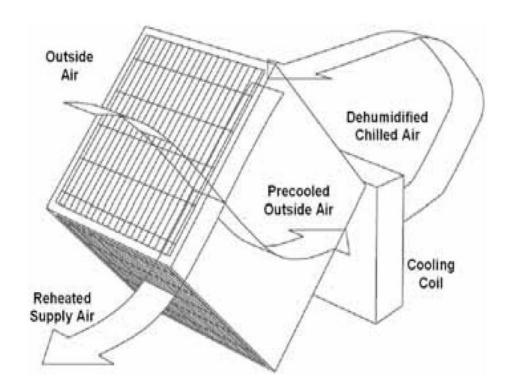






Using Air-to-Air HX to Super-Charge a Dehumidifier

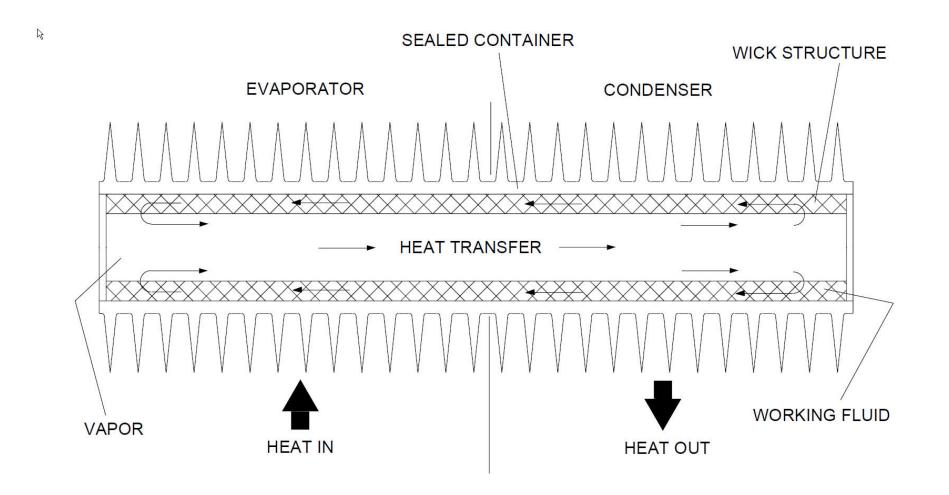
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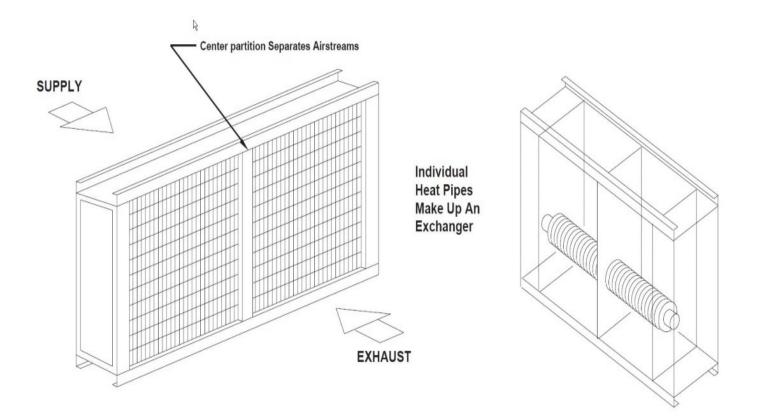
Heat Pipe Inner Workings







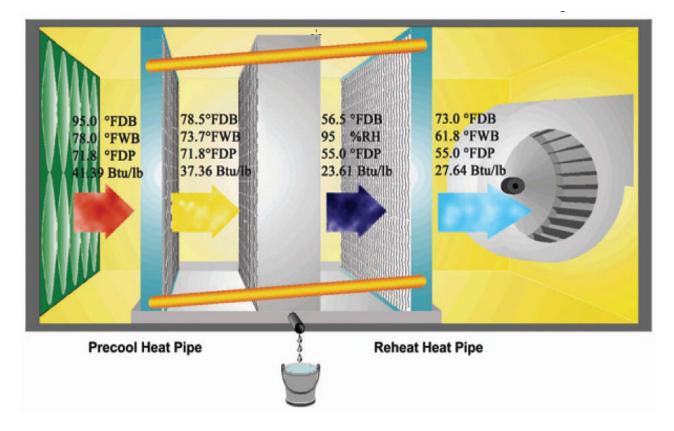
Heat Pipes in Side-by-Side Heat Recovery Arrangement







Heat Pipes used to supercharge dehumidification

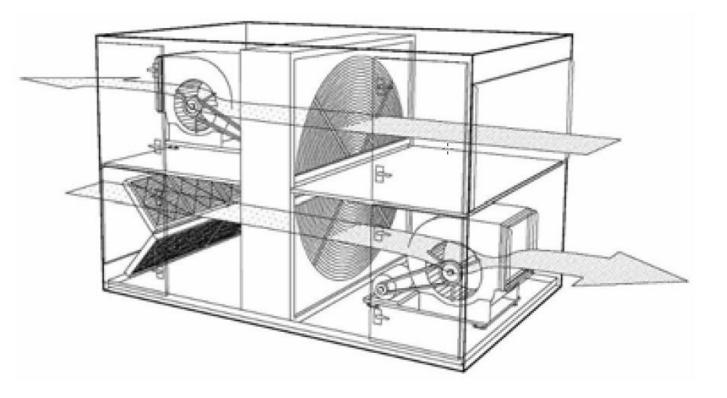






Heat Wheel Make-Up Air Heat Recovery Unit

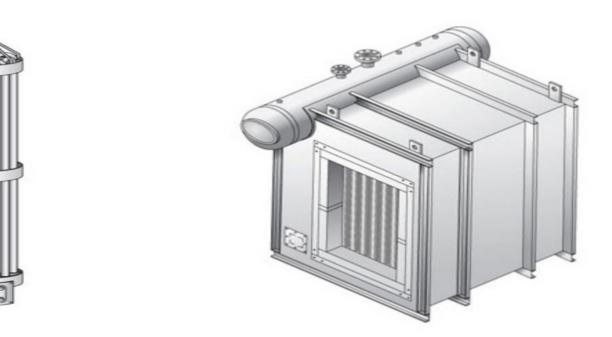
- Wheel can be made of porous material to recover latent heat
- Wheels made of
 - Fibrous paperboard
 - Silica gel
- Large silica gel wheels can be very heavy







Air to Water



Flue Gas Heat Recovery Tube Bundle

Heat Recovery Steam Generator





Water to Air



 Easiest heat recovery id when there is hot water already available from a process, such as watercooled ductwork, furnace jacket water, etc.





Key Points / Action Items



- . Based on the situation analyze suitable optimization opportunities, i.e. new fan, VFD, belt ration change, etc.
- 2. Look at thermal opportunities for heat recovery
- 3. Once gaps are identified, delve into more detail using the other US DOE's tools and resources
- 4. Quantify, prioritize, implement and continue to monitor





Homework #7

 Use the MEASUR tool to analyze the data for one of your fans, or the cement kiln ID fan data that was provided a few weeks ago.

Develop optimization opportunities as appropriate for the system

- Reduce wasteful pressure loss
- Reduce unnecessary flow (i.e. leaks)
- Use a more efficient control method for the fan
- Use a more efficient configuration of the fan, i.e. new belts and pulleys, tip/de-tip, replacement fan, replacement impeller





Thank You all for attending today's webinar.

See you all on next Thursday –

If you have specific questions, please stay online and we will try and answer them.

Alternately, you can email questions to me at ron@productiveenergy.com

